

CEQA Hydrology & Hydraulics Study

**Jamul Highlands Road
Jamul, California**

APN: 596-152-04-00

PDS2015-TPM-21255

Prepared For

**William Roetzheim
13518 Jamul Drive
Jamul, California 91935
Phone: 619-917-4917**

Prepared By

**Landmark Engineering Corporation
Lawrence E. Cole, RCE 36292
3443 Camino Del Rio South #204
San Diego, California 92108
Phone 619-260-0420**

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Lawrence E. Cole, RCE 36292
Exp. 06/30/20

Date



Project #2393

April 03, 2019

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FEMA FIRMETTE – 06073C1955G

DRAINAGE MAPS

DRAINAGE MAP (EXISTING)
DRAINAGE MAP (PROPOSED)
COUNTY 200 SCALE (AREA AROUND SITE)

INTRODUCTION

The proposed project site is located in the County of San Diego. The project is located at on the west side of Jamul Highlands Road between Highland Heights Road and Paleo Drive in Jamul, County of San Diego. The overall project site is Parcel 4 of Parcel Map 6976 and is undeveloped. It is bordered to the east by Jamul Highlands Road and to the north, south, and west by existing single family residences. The Assessor's Parcel number for the project lot is APN 596-152-04-00. The project proposes grading and improvements for a new single family residence. This drainage study calculates the peak stormwater discharge entering and leaving the project site (onsite and offsite drainage) in the existing condition and after development.

PROJECT SITE DESCRIPTION

The area of the project site is 458,791.992 s.f. (10.532 acres). The watershed soil is categorized as "Soil Group C". The existing area of the site is undeveloped thus $C = 0.30$. The area of the new driveway surface (impervious) is 34,332.8 square feet (0.788 acres). The area of the new home surface (impervious) is 9785.0 square feet (0.225 acres). The proposed impervious area of the site is than 11.8% thus $C = 0.36$ for disturbed or developed portions of the project site.

METHODOLOGY

Stormwater runoff was calculated using the Rational Method as outlined in the San Diego County Hydrology Manual, dated June 2003. Stormwater runoff was calculated for an existing and post-development condition resulting from the 100-year, 6-hour storm event for the project and its drainage area. Standard intensity-duration curve data was used for the San Diego region supplied in the Manual.

The soil group used for the site and in the drainage area is soil hydrologic Group C from Map Soil Hydrology Groups in County Hydrology Manual.

EXISTING CONDITION HYDROLOGY

The existing project site drainage area is approximately 19.418 acres. The site varies in elevation from a high of 1492 on north property line to a low at the southwest corner of the property. The calculation, the 19.418 acre drainage area in the existing condition is divided into 23 separate basins (See Drainage Map (Existing)) each described as follows:

Area E1 a portion of existing Jamul Highlands Road, a portion of the property on the west side of Jamul Highlands Road, and a small portion of the driveway which provides access. The stormwater does not flow into the proposed project. The developed street intercepts the flow and carries the stormwater southerly away from the site in the existing street gutters. No stormwater flows into the proposed project. Jamul Highlands Road collects the flow and carries the stormwater southerly away from the site in the existing street gutters. For this portion, since improved portions offsite, use C = 0.61.

Area E2 is a portion on the north side of the driveway. The stormwater will be collected in an 18" culvert and carried under the driveway into Area P7. This area provides for the proper design of the culvert and rip-rap energy dissipater. The area is self-mitigating and has no impervious areas. Use C = 0.36.

Area E3 is a portion on the north side of the driveway. The stormwater will be collected in an 18" culvert and carried under the driveway into Area P7. This area provides for the proper design of the culvert and rip-rap energy dissipater. The area is self-mitigating and has no impervious areas. Use C = 0.36.

Area E4 is a portion on the north side of the driveway. The stormwater will be collected in an 18" culvert and carried under the driveway into Area P8. This area provides for the proper design of the culvert and rip-rap energy dissipater. The area is self-mitigating and has no impervious areas. Use C = 0.30.

Area E5 consists of a portion which is redefined due to grading for the single family residence. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.30.

Area E6 consists of portion which is redefined due to grading for the single family residence. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.30.

Area E7 is a portion on the south side of the driveway. Stormwater from Area E2 and Area E3 enters this area from the north. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.36.

EXISTING CONDITION HYDROLOGY (continued)

Area E8 is a portion on the south side of the driveway which will provide access and a portion of the driveway. Stormwater after detention enters this area from the north. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.30.

Area E9 is a portion Area E3 on the south side of the driveway. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.30.

Area E10 consists of a portion which is redefined due to grading for the single family residence. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.30.

Area E11 consists of a portion which is redefined due to grading for the single family residence. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.30.

Area E12 consists of a portion which is redefined due to grading for the single family residence. For this portion, which is self-mitigating, there is no impervious area. Use C = 0.30.

Area E13 is a portion which is graded for the single family residential pad and includes a portion of the roof. This area provides for proper design of area drain for the graded pad. For this portion, impervious area is 3863.690 sf or 29%. Use C = 0.47.

Area E14 is a portion which is due to grading the single family residential pad and includes a portion of the roof. This area provides for proper design of area drain for the graded pad. For this portion, impervious area is 1147.689 sf or 26%. Use C = 0.46.

Area E15 is a portion on the north side of the driveway and a portion of the roof. For this portion, impervious area is 15127.611 sf or 44%. Use C = 0.56.

Area E16 is a portion on the south side of the driveway. For this portion, impervious area is 11133.418 sf or 49%. Use C = 0.59.

Area E17 is a portion on the north side of the driveway. For this portion, impervious area is 6614.580 sf or 62%. Use C = 0.62.

Area E18 is a portion on the south side of the driveway. For this portion, impervious area is 6758.351 sf or 68%. Use C = 0.71.

Area E19 is an onsite drainage area that sheet drains southerly over the south boundary. There is no POC for this area. As there has been no development use C = 0.30.

Area E20 is an onsite drainage area and in which the stormwater sheet flows westerly over a natural slope to a POC along the west boundary of the property. As there has been no development use C = 0.30.

Area E21 is an onsite drainage area and in which the stormwater sheet flows westerly over a natural slope to a POC along the west boundary of the property. As there has been no development use C = 0.30.

Area E22 is a small portion onsite that sheet flows southerly over and from the project. There is no POC for this area.

EXISTING CONDITION HYDROLOGY (continued)

Area E23 is a portion of existing Jamul Highlands Road and a portion of the property on the east side of Jamul Highlands Road. The stormwater does not flow into the proposed project. The developed street intercepts the flow and carries the stormwater southerly away from the site in the existing street gutters. For this portion use C = 0.61.

METHODOLOGY (continued)

POST- DEVELOPMENT HYDROLOGY

The project site drainage area is approximately 19.418 acres.

The project proposes new grading or disturbance for three residential pads

The project does not propose any grading or additional disturbance of any of the remaining Areas (includes paved portion of Jamul Highlands Road.) Continue to use C's per existing descriptions.

The calculations for, the 3.373 acre drainage area that is graded or disturbed is divided into 3 separate basins (See Drainage Map (Proposed)) each described as follows:

Area P1 is grading and construction for a single family residence in Parcel 2. It includes portions of Area E10, Area E11, Area E12, and Area E5. Residual portions of the Areas are labeled E10R, E11R, E12R and E5R. Parcel 2 creates an estimated 9500 sf of impervious area or $9500/29893.212 = 30\%$. The C value due to increased impervious area increases from 0.30 to 0.48.

Area P2 is grading and construction for a single family residence in Parcel 3. It includes portions of Area E3 and Area E4. The residual portions of the Areas are labeled E3R and E4R. Parcel 3 creates an estimated 6000 sf of impervious area or $6000/ 9794.389 = 61\%$. The C value due to increased impervious area increases from 0.36 to 0.67.

Area P3 is grading and construction for a single family residence in Parcel 4. It includes portions of Area E7and Area E8. Residual portions of the Areas are labeled E7Rand E8R. Parcel 4 creates an estimated 3600 sf of impervious area or $3600/ 6942.815 = 52\%$. The C value due to increased impervious area increases from 0.30 to 0.61.

For this project $L_m = 85$ and $T_i = 10.0$ from Table 3-2. For conservative design typically used T_c of 5 min. and just oversized facilities.

HYDROLOGY CALCULATIONS

Area < 0.5 square miles. Use Rational Formula

$$Q_{100} = CIA$$

$$\phi = N32^\circ 43' 37''$$

$$\lambda = W116^\circ 50' 40''$$

From Hydrology Manual Soils Map - Soils Group C

Undisturbed Natural (Existing)

$$C = 0.30$$

Low Density Residential (LDR) (Proposed)

$$C = 0.36$$

From INTENSITY-DURATION DESIGN CHART

$$I_{100} = 8.69 \text{ in/hr.}$$

$$I_2 = 3.95 \text{ in/hr.}$$

From Existing Drainage Map

Area E1 = 0.142 acres

Area E2 = 7.262 acres

Area E3 = 2.142 acres

Area E4 = 2.037 acres

Area E5 = 1.375 acres

Area E6 = 0.042 acres

Area E7 = 0.550 acres

Area E8 = 0.794 acres

Area E9 = 0.699 acres

Area E10 = 0.245 acres

Area E11 = 0.134 acres

Area E12 = 0.437 acres

Area E13 = 0.303 acres

Area E14 = 0.103 acres

Area E15 = 0.796 acres

Area E16 = 0.517 acres

Area E17 = 0.245 acres

Area E18 = 0.228 acres

Area E19 = 0.357 acres

Area E20 = 0.535 acres

Area E21 = 0.123 acres

Area E22 = 0.026 acres

Area E23 = 0.094 acres

19.418 acres

HYDROLOGY CALCULATIONS (CONTINUED)

| | |
|-----------|---|
| Area E1: | $Q_{100} = CIA = (0.61)(8.69)(0.142) = 0.75 \text{ cfs}$ |
| Area E2: | $Q_{100} = CIA = (0.36)(8.69)(7.262) = 22.72 \text{ cfs}$ |
| Area E3: | $Q_{100} = CIA = (0.36)(8.69)(2.142) = 6.70 \text{ cfs}$ |
| Area E4: | $Q_{100} = CIA = (0.30)(8.69)(2.037) = 5.31 \text{ cfs}$ |
| Area E5: | $Q_{100} = CIA = (0.30)(8.69)(1.375) = 3.58 \text{ cfs}$ |
| Area E6: | $Q_{100} = CIA = (0.30)(8.69)(0.042) = 0.11 \text{ cfs}$ |
| Area E7: | $Q_{100} = CIA = (0.36)(8.69)(0.550) = 1.72 \text{ cfs}$ |
| Area E8: | $Q_{100} = CIA = (0.30)(8.69)(0.794) = 2.07 \text{ cfs}$ |
| Area E9: | $Q_{100} = CIA = (0.30)(8.69)(0.699) = 1.82 \text{ cfs}$ |
| Area E10: | $Q_{100} = CIA = (0.30)(8.69)(0.245) = 0.64 \text{ cfs}$ |
| Area E11: | $Q_{100} = CIA = (0.30)(8.69)(0.134) = 0.35 \text{ cfs}$ |
| Area E12: | $Q_{100} = CIA = (0.30)(8.69)(0.437) = 1.14 \text{ cfs}$ |
| Area E13: | $Q_{100} = CIA = (0.47)(8.69)(0.303) = 1.24 \text{ cfs}$ |
| Area E14: | $Q_{100} = CIA = (0.46)(8.69)(0.103) = 0.41 \text{ cfs}$ |
| Area E15: | $Q_{100} = CIA = (0.56)(8.69)(0.796) = 3.87 \text{ cfs}$ |
| Area E16: | $Q_{100} = CIA = (0.59)(8.69)(0.517) = 2.65 \text{ cfs}$ |
| Area E17: | $Q_{100} = CIA = (0.62)(8.69)(0.245) = 1.32 \text{ cfs}$ |
| Area E18: | $Q_{100} = CIA = (0.71)(8.69)(0.228) = 1.41 \text{ cfs}$ |
| Area E19: | $Q_{100} = CIA = (0.30)(8.69)(0.357) = 0.93 \text{ cfs}$ |
| Area E20: | $Q_{100} = CIA = (0.30)(8.69)(0.535) = 1.39 \text{ cfs}$ |
| Area E21: | $Q_{100} = CIA = (0.30)(8.69)(0.354) = 0.92 \text{ cfs}$ |
| Area E22: | $Q_{100} = CIA = (0.30)(8.69)(0.026) = 0.07 \text{ cfs}$ |
| Area E23: | $Q_{100} = CIA = (0.61)(8.69)(0.094) = \underline{0.50 \text{ cfs}}$ 61.62 cfs |

HYDROLOGY CALCULATIONS (CONTINUED)

| | |
|-----------|---|
| Area E1: | $Q_2 = CIA = (0.61)(3.95)(0.142) = 0.34 \text{ cfs}$ |
| Area E2: | $Q_2 = CIA = (0.36)(3.95)(7.262) = 18.33 \text{ cfs}$ |
| Area E3: | $Q_2 = CIA = (0.36)(3.95)(2.142) = 3.05 \text{ cfs}$ |
| Area E4: | $Q_2 = CIA = (0.30)(3.95)(2.037) = 2.41 \text{ cfs}$ |
| Area E5: | $Q_2 = CIA = (0.30)(3.95)(1.375) = 1.63 \text{ cfs}$ |
| Area E6: | $Q_2 = CIA = (0.30)(3.95)(0.042) = 0.05 \text{ cfs}$ |
| Area E7: | $Q_2 = CIA = (0.36)(3.95)(0.550) = 0.78 \text{ cfs}$ |
| Area E8: | $Q_2 = CIA = (0.30)(3.95)(0.794) = 0.94 \text{ cfs}$ |
| Area E9: | $Q_2 = CIA = (0.30)(3.95)(0.699) = 0.83 \text{ cfs}$ |
| Area E10: | $Q_2 = CIA = (0.30)(3.95)(0.245) = 0.29 \text{ cfs}$ |
| Area E11: | $Q_2 = CIA = (0.30)(3.95)(0.134) = 0.16 \text{ cfs}$ |
| Area E12: | $Q_2 = CIA = (0.30)(3.95)(0.437) = 0.52 \text{ cfs}$ |
| Area E13: | $Q_2 = CIA = (0.47)(3.95)(0.303) = 0.56 \text{ cfs}$ |
| Area E14: | $Q_2 = CIA = (0.46)(3.95)(0.103) = 0.19 \text{ cfs}$ |
| Area E15: | $Q_2 = CIA = (0.56)(3.95)(0.796) = 1.76 \text{ cfs}$ |
| Area E16: | $Q_2 = CIA = (0.59)(3.95)(0.517) = 1.20 \text{ cfs}$ |
| Area E17: | $Q_2 = CIA = (0.62)(3.95)(0.245) = 0.60 \text{ cfs}$ |
| Area E18: | $Q_2 = CIA = (0.71)(3.95)(0.228) = 0.64 \text{ cfs}$ |
| Area E19: | $Q_2 = CIA = (0.30)(3.95)(0.357) = 0.51 \text{ cfs}$ |
| Area E20: | $Q_2 = CIA = (0.30)(3.95)(0.535) = 0.76 \text{ cfs}$ |
| Area E21: | $Q_2 = CIA = (0.30)(3.95)(0.354) = 0.50 \text{ cfs}$ |
| Area E22: | $Q_2 = CIA = (0.30)(3.95)(0.026) = 0.04 \text{ cfs}$ |
| Area E23: | $Q_2 = CIA = (0.61)(3.95)(0.094) = \underline{0.23 \text{ cfs}}$ 36.32 cfs |

HYDROLOGY CALCULATIONS (CONTINUED)

Post-Construction

| | |
|------------|--|
| Area P1: | $Q_{100} = CIA = (0.48)(8.69)(0.686) = 2.86 \text{ cfs}$ |
| Area E10R: | $Q_{100} = CIA = (0.30)(8.69)(0.151) = 0.39 \text{ cfs}$ |
| Area E11R: | $Q_{100} = CIA = (0.30)(8.69)(0.048) = 0.13 \text{ cfs}$ |
| Area E12R: | $Q_{100} = CIA = (0.30)(8.69)(0.079) = 0.21 \text{ cfs}$ |
| Area E5R: | $Q_{100} = CIA = (0.30)(8.69)(1.226) = 3.20 \text{ cfs}$ |
| | |
| Area P2: | $Q_{100} = CIA = (0.67)(8.69)(0.225) = 1.31 \text{ cfs}$ |
| Area E3R: | $Q_{100} = CIA = (0.30)(8.69)(1.935) = 5.04 \text{ cfs}$ |
| Area E4R: | $Q_{100} = CIA = (0.30)(8.69)(2.034) = 5.30 \text{ cfs}$ |
| | |
| Area P3: | $Q_{100} = CIA = (0.61)(8.69)(0.159) = 0.84 \text{ cfs}$ |
| Area E7R: | $Q_{100} = CIA = (0.30)(8.69)(0.531) = 1.38 \text{ cfs}$ |
| Area E8R: | $Q_{100} = CIA = (0.30)(8.69)(0.654) = \frac{1.70 \text{ cfs}}{22.36 \text{ cfs}}$ |
| | |
| Area P1: | $Q_2 = CIA = (0.48)(3.95)(0.686) = 1.30 \text{ cfs}$ |
| Area E10R: | $Q_2 = CIA = (0.30)(3.95)(0.151) = 0.18 \text{ cfs}$ |
| Area E11R: | $Q_2 = CIA = (0.30)(3.95)(0.048) = 0.06 \text{ cfs}$ |
| Area E12R: | $Q_2 = CIA = (0.30)(3.95)(0.079) = 0.09 \text{ cfs}$ |
| Area E5R: | $Q_2 = CIA = (0.30)(3.95)(1.226) = 1.45 \text{ cfs}$ |
| | |
| Area P2: | $Q_2 = CIA = (0.67)(3.95)(0.225) = 0.60 \text{ cfs}$ |
| Area E3R: | $Q_2 = CIA = (0.30)(3.95)(1.935) = 2.29 \text{ cfs}$ |
| Area E4R: | $Q_2 = CIA = (0.30)(3.95)(2.034) = 2.41 \text{ cfs}$ |
| | |
| Area P3: | $Q_2 = CIA = (0.61)(3.95)(0.159) = 0.38 \text{ cfs}$ |
| Area E7R: | $Q_2 = CIA = (0.30)(3.95)(0.531) = 0.63 \text{ cfs}$ |
| Area E8R: | $Q_2 = CIA = (0.30)(3.95)(0.654) = \frac{0.77 \text{ cfs}}{10.16 \text{ cfs}}$ |

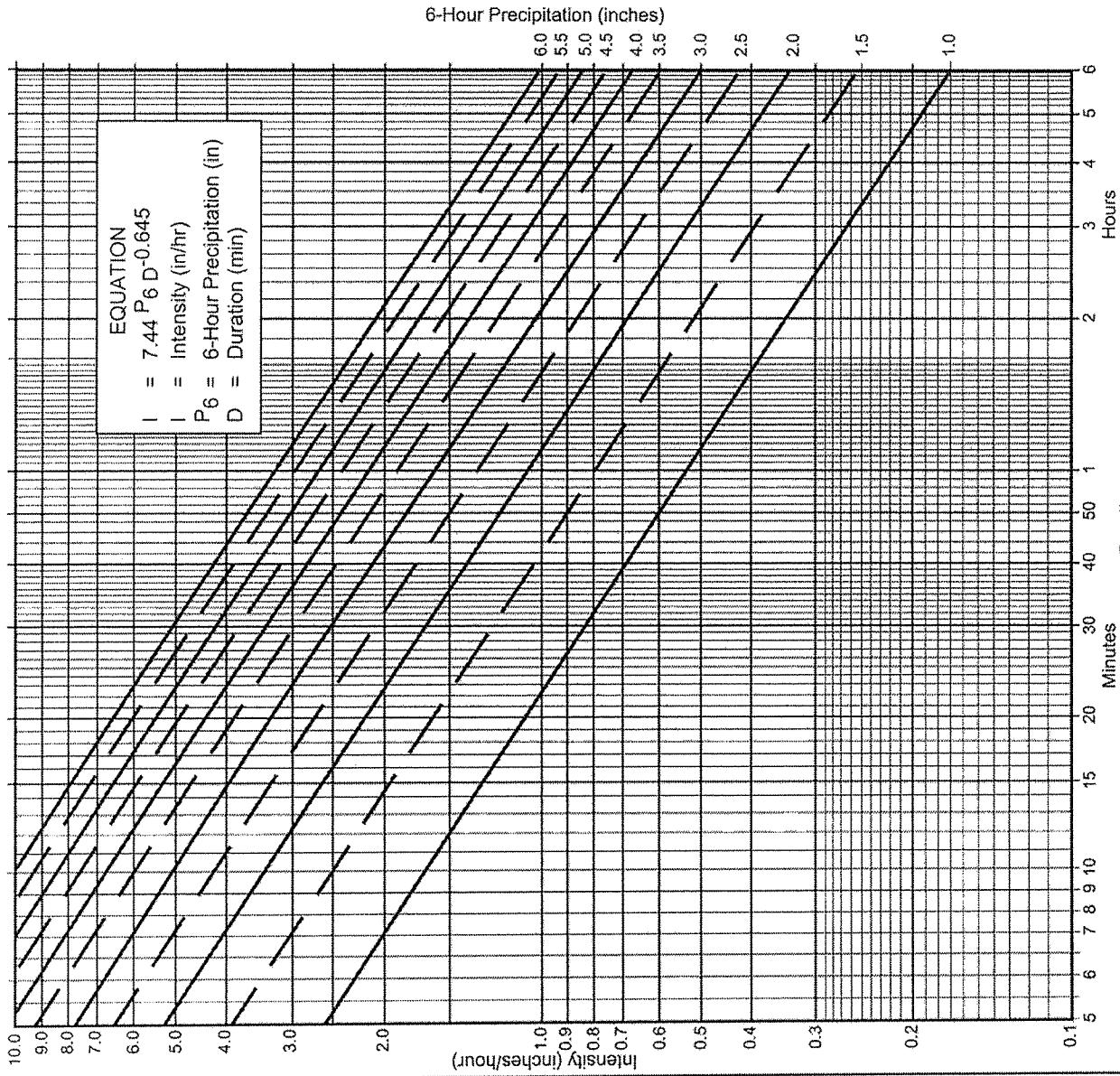
Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency 100 year
- (b) $P_6 = \frac{3.3}{P_{24}} \text{ in.}$, $P_{24} = \frac{7.1}{P_6} \text{ in.}$
- (c) Adjusted $P_6^{(2)} = \frac{3.3}{P_{24}}$ in.
- (d) $t_X = \frac{5}{P_6}$ min.
- (e) $I = \frac{8.69}{t_X}$ in./hr. Calculated by formula

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.



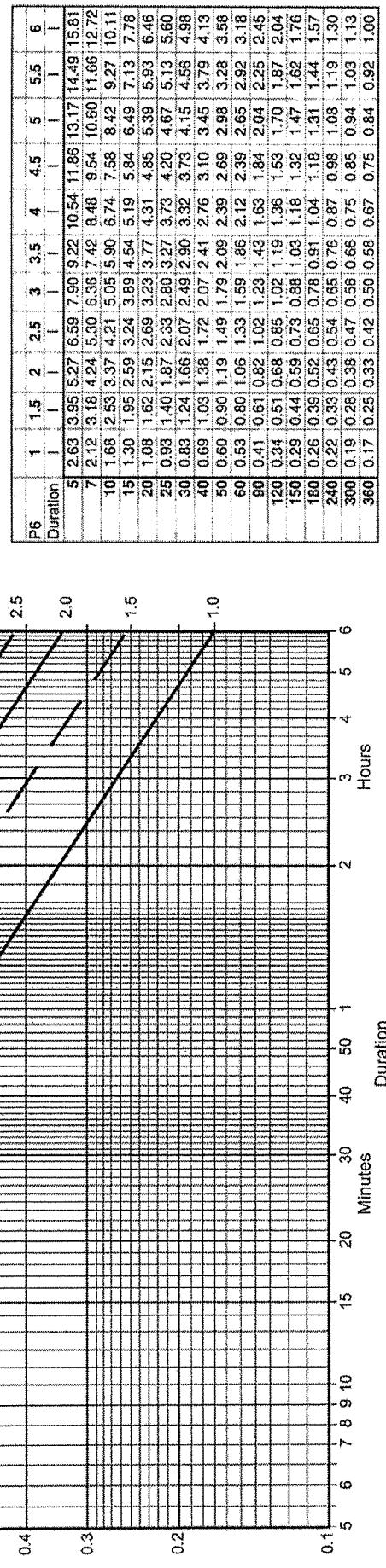
Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency 2 year
 $P_6 = \frac{1.5}{P_{24}} P_{24} = \frac{2.5}{P_{24}} = 60\% (2)$
- (b) $P_6 = \frac{1.5}{in.}$, $P_{24} = \frac{2.5}{in.}$
- (c) Adjusted $P_6^{(2)} = \frac{1.5}{in.}$
- (d) $t_x = \frac{5}{min.}$
- (e) $I = \frac{3.95}{in./hr.}$ Calculated by formula

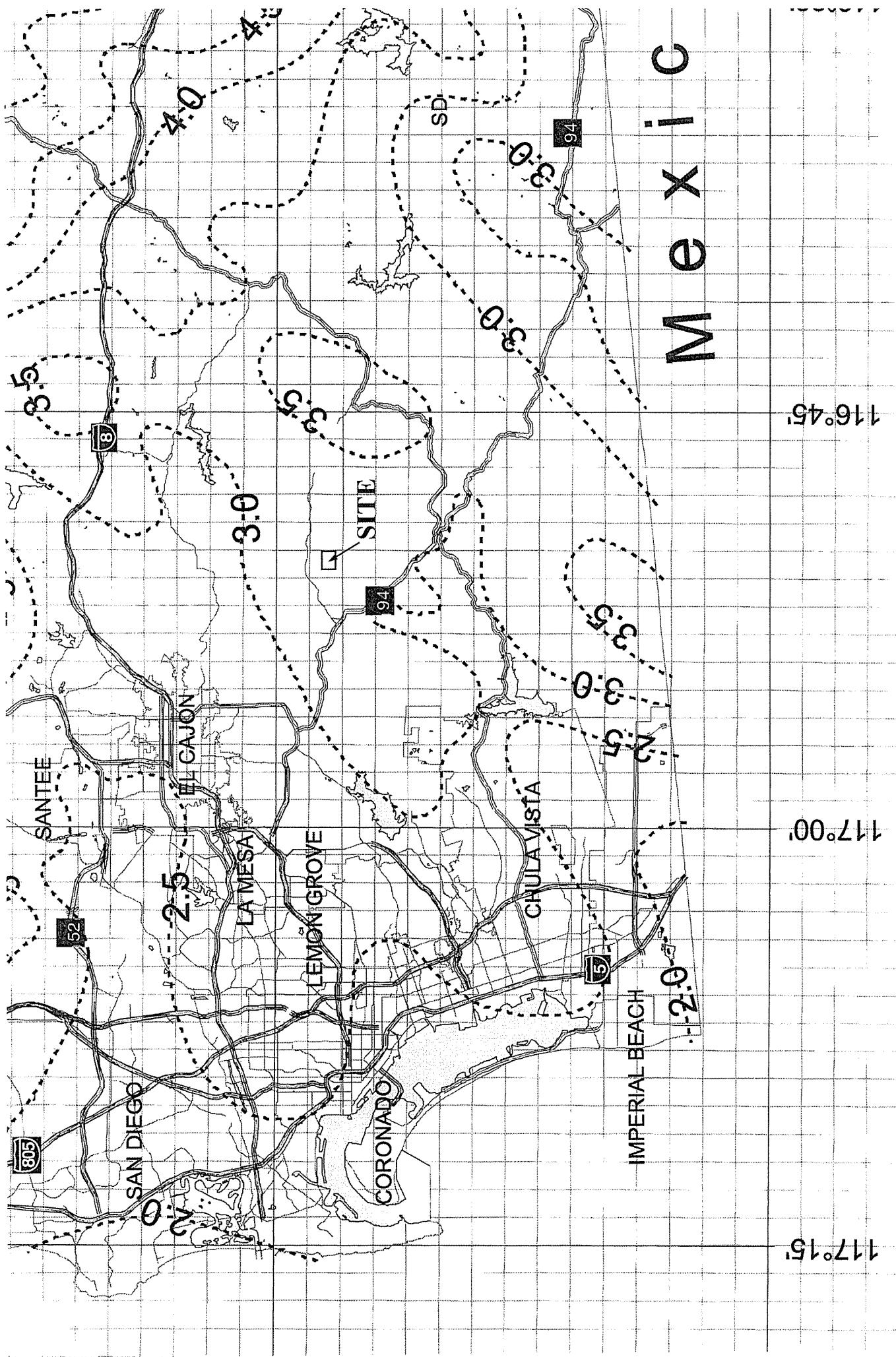
Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.



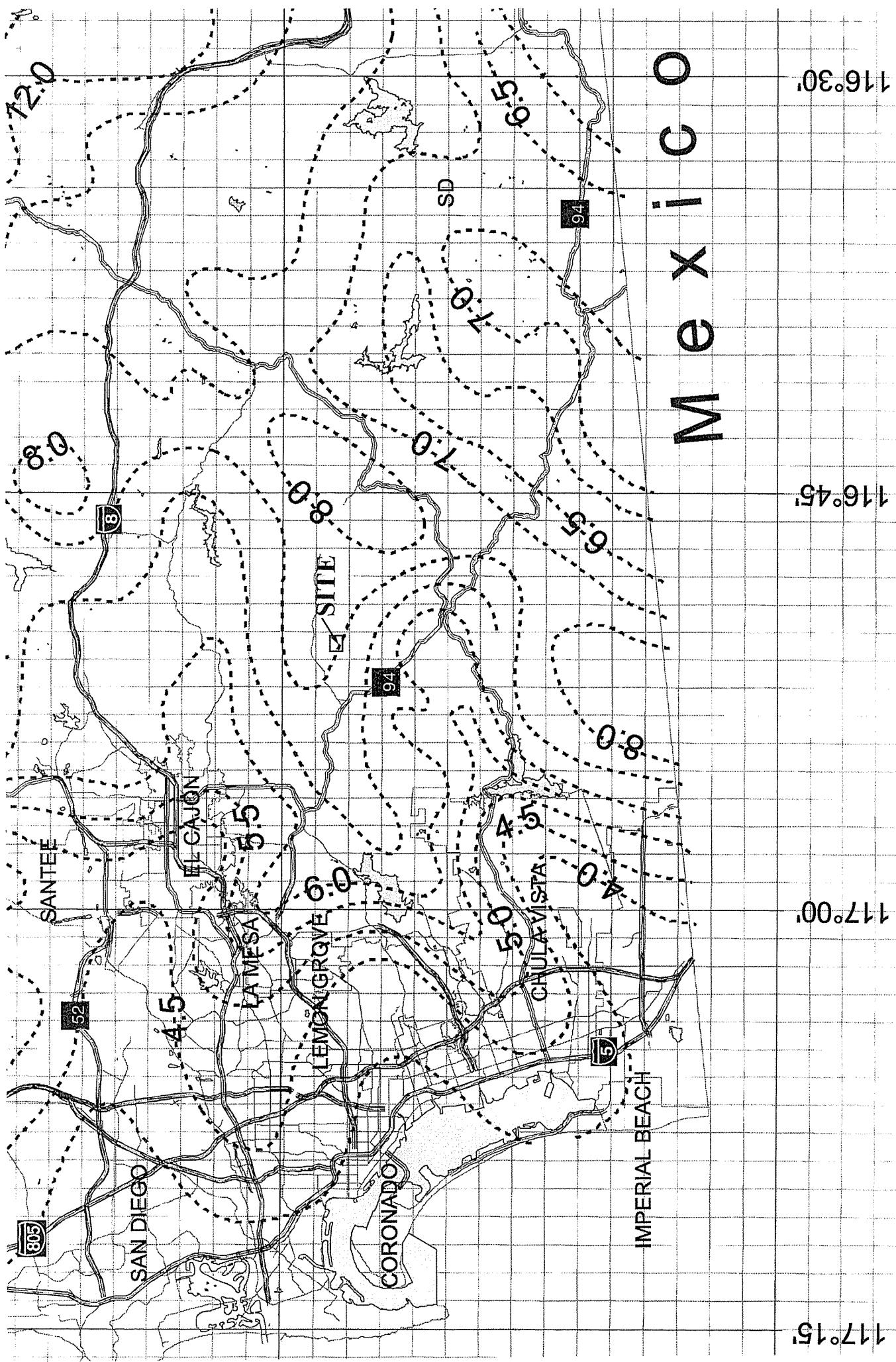
FIGURE

Intensity-Duration Design Chart - Template

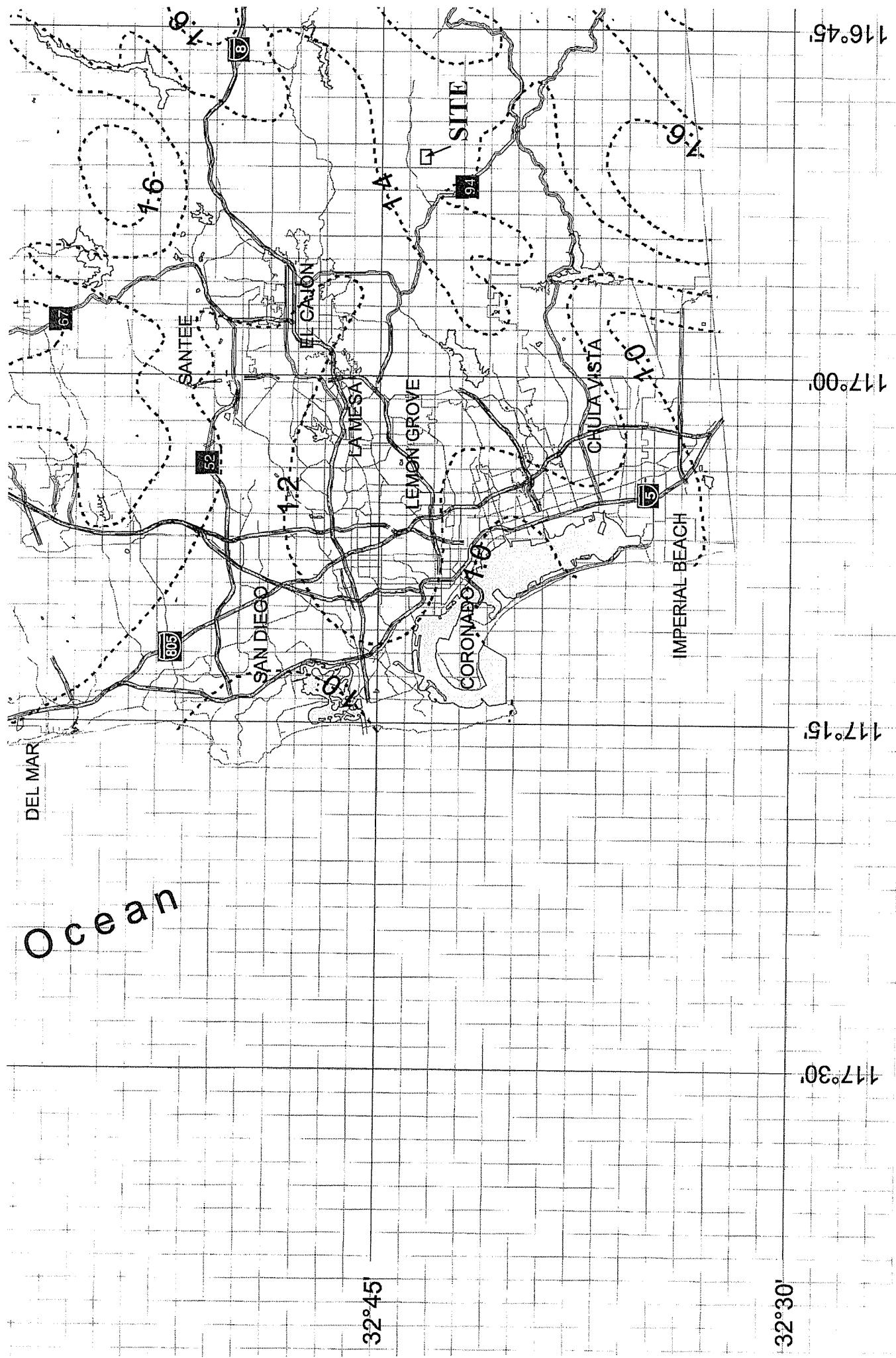
3-1

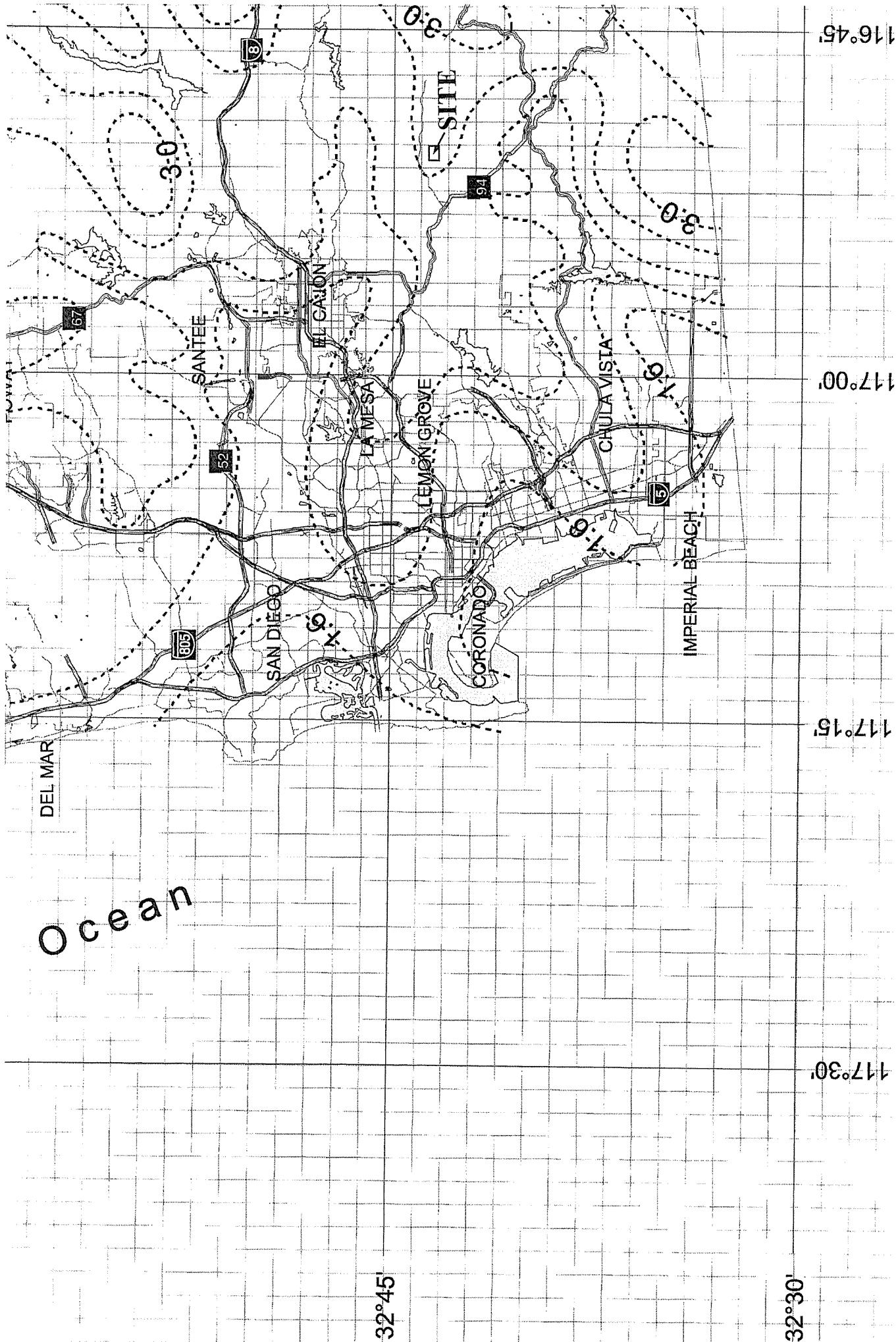


100-year 6-hour



100-year 24-hour





2-year 24-hour

Table 3-1
RUNOFF COEFFICIENTS FOR URBAN AREAS

| NRCS Elements | Land Use | County Elements | Runoff Coefficient "C" | | | |
|---------------------------------------|--------------------------------|-----------------|------------------------|------|------|------|
| | | | % IMPER. | A | B | C |
| Undisturbed Natural Terrain (Natural) | Permanent Open Space | (0*) | 0.20 | 0.25 | 0.30 | 0.35 |
| Low Density Residential (LDR) | Residential, 1.0 DU/A or less | (10) | 0.27 | 0.32 | 0.36 | 0.41 |
| Low Density Residential (LDR) | Residential, 2.0 DU/A or less | 20 | 0.34 | 0.38 | 0.42 | 0.46 |
| Low Density Residential (LDR) | Residential, 2.9 DU/A or less | 25 | 0.38 | 0.41 | 0.45 | 0.49 |
| Medium Density Residential I (MDR) | Residential, 4.3 DU/A or less | 30 | 0.41 | 0.45 | 0.48 | 0.52 |
| Medium Density Residential (MDR) | Residential, 7.3 DU/A or less | 40 | 0.48 | 0.51 | 0.54 | 0.57 |
| Medium Density Residential (MDR) | Residential, 10.9 DU/A or less | 45 | 0.52 | 0.54 | 0.57 | 0.60 |
| Medium Density Residential (MDR) | Residential, 14.5 DU/A or less | 50 | 0.55 | 0.58 | 0.60 | 0.63 |
| High Density Residential (HDR) | Residential, 24.0 DU/A or less | 65 | 0.66 | 0.67 | 0.69 | 0.71 |
| High Density Residential (HDR) | Residential, 43.0 DU/A or less | 80 | 0.76 | 0.77 | 0.78 | 0.79 |
| Commercial/Industrial (N. Com) | Neighborhood Commercial | 80 | 0.76 | 0.77 | 0.78 | 0.79 |
| Commercial/Industrial (G. Com) | General Commercial | 85 | 0.80 | 0.80 | 0.81 | 0.82 |
| Commercial/Industrial (O.P. Com) | Office Professional/Commercial | 90 | 0.83 | 0.84 | 0.84 | 0.85 |
| Commercial/Industrial (Limited I.) | Limited Industrial | 90 | 0.83 | 0.84 | 0.84 | 0.85 |
| Commercial/Industrial (General I.) | General Industrial | 95 | 0.87 | 0.87 | 0.87 | 0.87 |

*The values associated with 0% impervious may be used for direct calculation of the runoff coefficient as described in Section 3.1.2 (representing the previous runoff coefficient, Cp, for the soil type), or for areas that will remain undisturbed in perpetuity. Justification must be given that the area will remain natural forever (e.g., the area is located in Cleveland National Forest).

DU/A = dwelling units per acre

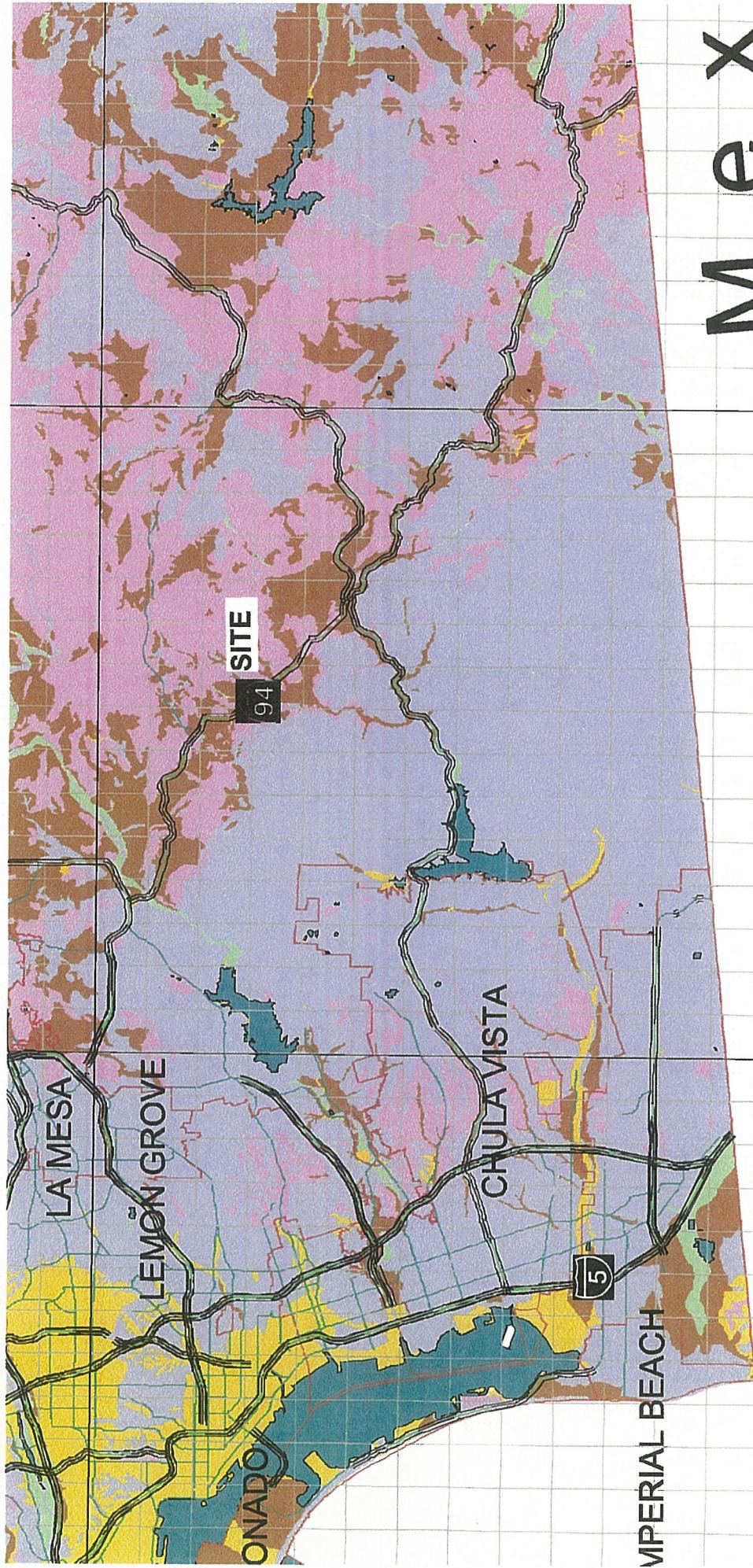
NRCS = National Resources Conservation Service

COUNTY SOILS MAP

M e X

116°45'

117°00'



HYDROLOGY CALCULATIONS SUMMARY

EXPECTED RUNOFF DISCHARGES

| Basin | C | | Tc | | A (acres) | |
|-------|------|------|--------|--------|--------------|--------|
| | Pre | Post | Pre | Post | Pre | Post |
| POC#1 | 0.30 | 0.30 | 5 min. | 5 min. | 1.375 | 1.226 |
| POC#2 | 0.30 | 0.30 | 5 min. | 5 min. | 0.437 | 0.079 |
| POC#3 | 0.30 | 0.30 | 5 min. | 5 min. | 0.134 | 0.048 |
| POC#4 | 0.30 | 0.30 | 5 min. | 5 min. | 0.245 | 0.151 |
| POC#5 | 0.30 | 0.30 | 5 min. | 5 min. | 14.589 | 14.231 |

EXPECTED RUNOFF DISCHARGES

| Basin | V ₁₀₀ (fps) | | Q ₁₀₀ Unmitigated with pads (cfs) | | Q ₁₀₀ Mitigated without pads (cfs) | |
|-------|---------------------------|------|---|--------|--|-------|
| | Pre | Post | Pre | Post | Pre | Post |
| POC#1 | 1.52 | 2.99 | 3.58 | 4.65 | 3.58 | 3.20 |
| POC#2 | 1.04 | 2.03 | 1.14 | 1.48 | 1.14 | 0.21 |
| POC#3 | 0.52 | 1.64 | 0.35 | 0.46 | 0.35 | 0.13 |
| POC#4 | 1.36 | 2.35 | 0.64 | 0.75 | 0.64 | 0.39 |
| POC#5 | 4.47 | 4.84 | 46.71 | 50.69 | 46.71 | 44.39 |
| Basin | C | | Tc | | A (acres) | |
| | Pre | Post | Pre | Post | Pre | Post |
| P1 | 0.30 | 0.48 | 5 min. | 5 min. | 0.686 | 0.686 |
| P2 | 0.30 | 0.64 | 5 min. | 5 min. | 0.245 | 0.245 |
| P3 | 0.30 | 0.77 | 5 min. | 5 min. | 0.113 | 0.113 |
| Total | N/A | N/A | N/A | N/A | 1.044 | 1.373 |

| Basin | V ₁₀₀ (fps) | | Q ₁₀₀ unmitigated (cfs) | |
|-------|---------------------------|------|--|------|
| | Pre | Post | Pre | Post |
| P1 | 1.52 | 2.99 | 2.42 | 2.86 |
| P2 | 4.47 | 4.84 | 0.64 | 1.36 |
| P3 | 1.66 | 3.10 | 0.29 | 0.76 |
| Total | N/A | N/A | 3.35 | 3.98 |

TREE WELL STORAGE CALCULATION

Freeboard storage/foot (above soil) = 11.25 ft x 11.25 ft x 1ft = 127 cf/ft tree well
 Freeboard storage/foot (above soil) = 20 ft x 20 ft x 1ft = 400 cf/ft canopy

Parcel Storage Requirement

| | Parcel 2 | Parcel 3 | Parcel 4 |
|---|----------|----------|----------|
| Area | 0.686 | 0.225 | 0.159 |
| Q _{pre} | 2.42 | 0.59 | 0.41 |
| Q _{post} | 2.86 | 1.31 | 0.84 |
| Q _{post} - Q _{pre} | 0.44 | 0.72 | 0.43 |
| C _{post} | 0.48 | 0.67 | 0.61 |
| I _{req} = Q _{pre} /Area/C _{post} | $= 7.35$ | $= 3.91$ | $= 4.23$ |

From Figure 3-1

$$T_c \text{ required min.} = 6.5 \text{ min.} \quad = 17.3 \text{ min.} \quad = 15.3 \text{ min.}$$

| | | | |
|--------------------|---|---|---|
| #Tree Wells | 6 | 4 | 2 |
|--------------------|---|---|---|

| | | | |
|----------------------|---------|---------|--------|
| Area 11.25' x 11.25' | 762 sf | 508 sf | 254 sf |
| Area 20' x 20' | 2400 sf | 1600 sf | 800 sf |

$$\text{Storage}_{\text{req}} = T_c \times 60 \times Q_{\text{post}} = 1115.4 \text{ cf} \quad = 1359.8 \text{ cf} \quad = 771.1 \text{ cf}$$

$$\text{Storage}_{\text{req}}/\text{Tree Well} = 185.9 \text{ cf} \quad = 340.0 \text{ cf} \quad = 385.6 \text{ cf}$$

$$\text{Minimum depth Tree Well} = 1.46 \text{ ft} \quad = 2.68 \text{ ft} \quad = 3.34 \text{ ft}$$

$$\text{Minimum depth Canopy} = 0.46 \text{ ft} \quad = 0.85 \text{ ft} \quad = 0.96 \text{ ft}$$

**Use Tree Well Depth of 1.00 feet
For all Tree Wells**

HYDRAULIC CALCULATIONS

Area Drain 12"X12" private

$$A = Q/2 \text{ (sump condition)}$$

$$Q = 2A = 2.00 \text{ cfs}$$

Area: P13, P14

$$Q = 1.24 \text{ cfs}, 0.41 \text{ cfs}$$

Capacity Area Drain = 2.00 cfs > 1.24 cfs, 0.41 cfs area drains OK!

Circular Pipes

Area: E2

$$Q = 22.72 \text{ cfs}$$

18" PVC @ 4.33%

$$d = 18"$$

$$\text{Slope} = .0433$$

$$n = 0.012$$

$$A = 1.767 \text{ s.f.}$$

$$R = 0.375$$

$$\text{Wetted perimeter (full)} = 4.712'$$

Calculated capacity $Q_{100} = 23.74 \text{ cfs} > 22.72 \text{ cfs OK!}$

$$y = 1.17 A = 1.485 P = 3.260$$

$$V = Q/A = 22.72/1.485 = 15.3 \text{ fps}$$

Area: E3R

$$Q = 4.95 \text{ cfs}$$

18" PVC @ 9.54%

$$d = 18"$$

$$\text{Slope} = .0954$$

$$n = 0.012$$

$$A = 1.767 \text{ s.f.}$$

$$R = 0.375$$

$$\text{Wetted perimeter (full)} = 4.712'$$

Calculated capacity $Q_{100} = 35.24 \text{ cfs} > 4.95 \text{ cfs OK!}$

$$y = 0.41 A = 0.352 P = 1.582$$

$$V = Q/A = 6.70/0.352 = 19.0 \text{ fps}$$

Area: E4, E13, E14

$$Q = 6.96 \text{ cfs}$$

$$Q_{\text{Allow}} = 4.55 \text{ cfs}$$

12" PVC @ 1.0%

$$d = 12"$$

$$\text{Slope} = .01$$

$$n = 0.012$$

$$A = 0.785 \text{ s.f.}$$

$$R = 0.250$$

$$\text{Wetted perimeter (full)} = 3.142'$$

Calculated capacity $Q_{100} = 3.87 \text{ cfs} < 4.55 \text{ cfs OK!}$

$$y = 0.57 A = 0.616 P = 1.993$$

$$V = Q/A = 6.96/0.616 = 11.3 \text{ fps}$$

HYDRAULIC CALCULATIONS (CONTINUED)

RIP-RAP per Standard Specifications for Public Works (Green Book)

Area: E2

$Q = 22.72 \text{ cfs}$

18" PVC @ 4.33%

$y = 1.17 A = 1.485 P = 3.260$

$V = Q/A = 22.72/1.485 = 15.3 \text{ fps}$

Rock Class: 1 Ton

Thickness: 4.3

Upper Layer Filter Blanket: 1-1/2"

Lower Layer Filter Blanket: Sand

Area: E3

$Q = 6.70 \text{ cfs}$

18" PVC @ 9.54%

$y = 0.57 A = 0.616 P = 1.993$

$V = Q/A = 6.70/0.616 = 10.9 \text{ fps}$

Rock Class: 1/4 Ton

Thickness: 2.7

Upper Layer Filter Blanket: 3/4"

Lower Layer Filter Blanket: Sand

Area: E4, E13, E14

$Q = 3.87 \text{ cfs full flow}$

12" PVC @ 1.00%

$y = 1.00 A = 0.785 P = 3.142$

$V = Q/A = 3.87/0.785 = 4.93 \text{ fps}$

Rock Class: 1/4 Ton

Thickness: 2.7

Upper Layer Filter Blanket: 3/4"

Lower Layer Filter Blanket: Sand

CONCLUSION

1. The proposed project does not substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river. No flooding will occur due to development on- or off-site.
2. With no reduction in Time of Concentration, the peak Q is increased from 1.14 cfs to 2.24 cfs, or 1.10 cfs in Parcel 2, from 6.70 cfs to 7.26 cfs, or 0.56 cfs in Parcel 3, and from 2.07 cfs to 2.56 cfs, or 0.49 cfs in Parcel 4. Changes to POCs are tabulated below. The use of tree wells mitigates runoff from pads and yields less runoff at POCs post-construction compared to pre-construction. See tabulation of POCs below.
3. There are thirty-five (35) existing tree wells that have been provided to address WQ/HMP requirements (See SWQMP). An additional eleven (11) are proposed for the three new Parcels to mitigate new roofs, driveways and impervious areas. They will mitigate any increases in runoff due to development of the project.
4. The proposed project would not place housing or structures within a 100-year hazard (See Firmette in Attachments), or expose people or structures to significant risk of loss, injury or death involving flooding.
5. The proposed project does not substantially alter the existing drainage pattern of the site and with the onsite mitigation of flow increases due to new impervious area no substantial erosion or siltation on-site or off-site is anticipated.
6. The proposed project does not substantially alter the existing drainage pattern of the site and with the onsite mitigation of flow increases due to new impervious area no on-site or off-site flooding is anticipated.
7. The proposed project does not create or contribute runoff water which would exceed the capacity of the existing or planned storm water drainage systems. The impervious roadway was mitigated with the original grading for Parcel 1 and proposed mitigation is added for smaller areas of Parcels 2, 3 and 4.
8. The proposed project does not propose any levees or dams with a potential for failing and not therefore expose people or structures to a significant risk of loss, injury or death involving flooding.

CONCLUSION (continued)

9. Hydrology Report Summary:

EXPECTED RUNOFF DISCHARGES @ 5 minutes (with mitigation)

| Outlet | Tributary Area (Acres) | | Q100 Peak Discharge (cfs) | | Q2 Peak Discharge (cfs) | |
|----------------------|---------------------------|--------|------------------------------|-------|----------------------------|-------|
| | Pre | Post | Pre | Post | Pre | Post |
| Jamul Highlands Road | 0.144 | 0.142 | 0.76 | 0.75 | 0.35 | 0.34 |
| POC#1 | 1.375 | 1.226 | 3.58 | 3.20 | 1.63 | 1.45 |
| POC#2 | 0.437 | 0.079 | 1.14 | 0.21 | 0.52 | 0.10 |
| POC#3 | 0.134 | 0.048 | 0.35 | 0.13 | 0.16 | 0.06 |
| POC#4 | 0.245 | 0.151 | 0.64 | 0.39 | 0.29 | 0.18 |
| POC#5 | 14.589 | 14.231 | 46.71 | 44.00 | 21.23 | 20.00 |

Outlets shown are based on changes per development of the project site.

Stormwater runoff was calculated using the Rational Method as outlined in the San Diego County Hydrology Manual, dated June 2003. Stormwater runoff was calculated for an existing and post-development condition resulting from the 100-year, 6-hour storm event for the project and its drainage area. Standard intensity-duration curve data was used for the San Diego region supplied in the Manual.

*POC#1 is the only one which requires mitigation to reduce Post to below Pre. See conclusion no. 2 above.

CERTIFICATION

Report Preparation

I certify that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to ensure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system or those persons directly responsible for gathering the information, to the best of my knowledge and belief, the information submitted is true, accurate, and complete.

CIVIL ENGINEER

Lawrence E. Cole, RCE 36292

April 03, 2019

Date



REFERENCES

1. County of San Diego Department of Public Works Flood Control Section, *San Diego County Hydrology Manual* dated June 2003.
2. County of San Diego *Stormwater Standards Manual*.

DECLARATION OF RESPONSIBLE CHARGE

I HEREBY DECLARE THAT I AM THE ENGINEER OF WORK FOR THIS PROJECT, THAT I HAVE EXERCISED RESPONSIBLE CHARGE OVER THE DESIGN OF THE PROJECT AS DEFINED IN SECTION 6703 OF THE BUSINESS AND PROFESSIONS CODE, AND THAT THE DESIGN IS CONSISTANT WITH CURRENT STANDARDS.

I UNDERSTAND THAT THE CHECK OF PROJECT DRAWINGS AND SPECIFICATIONS BY COUNTY OF SAN DIEGO IS CONFINED TO A REVIEW ONLY AND DOES NOT RELIEVE ME, AS ENGINEER OF WORK, OF MY RESPONSIBILITIES FOR PROJECT DESIGN.

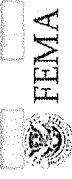
April 03, 2019

Lawrence E. Cole, RCE 36292
EXP. 06/30/20

Date



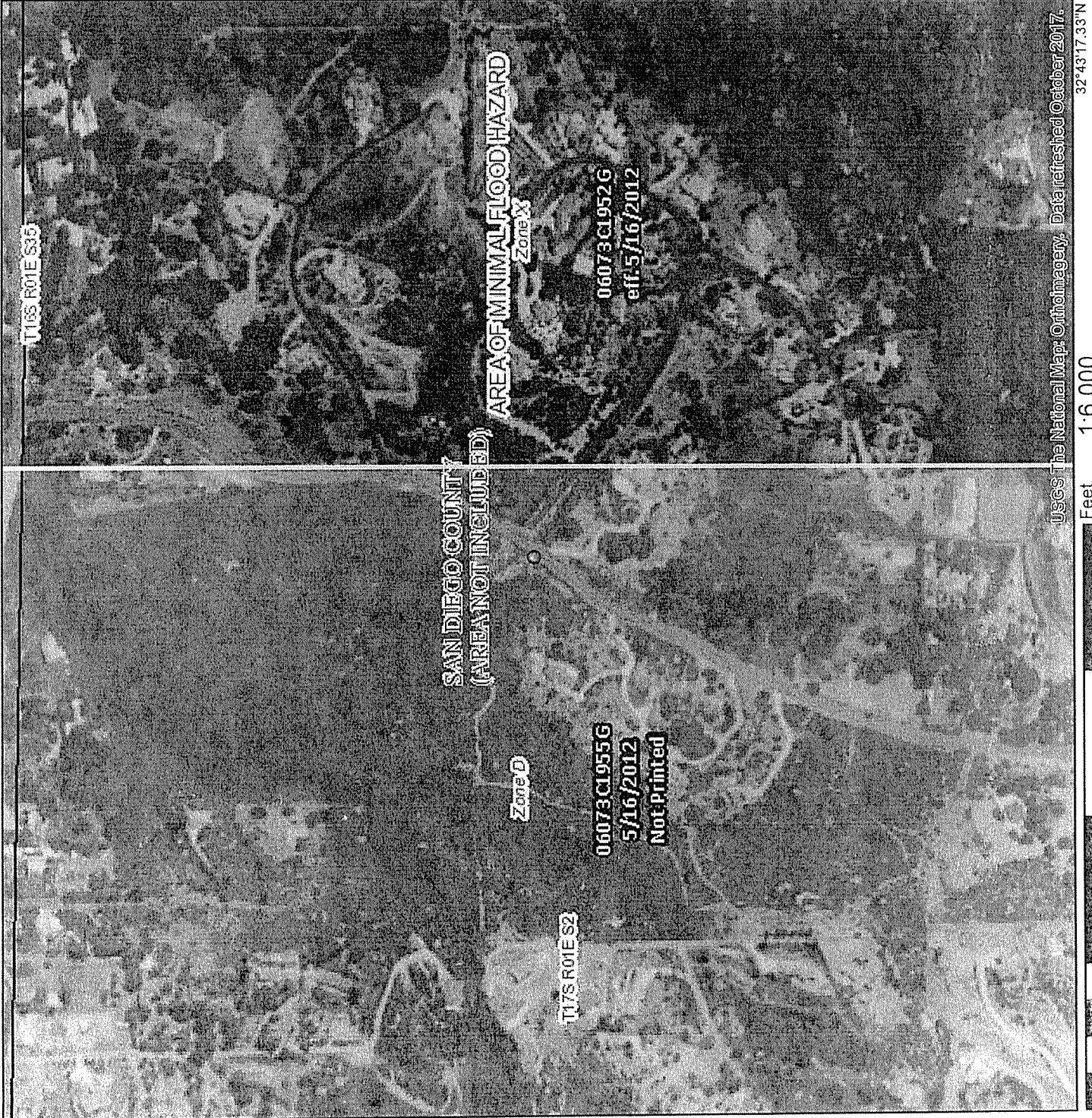
National Flood Hazard Layer FIRMap



Legend

2434.7.60°N

SEE THIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below.

The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHIL web services provided by FEMA. This map was exported on 10/8/2018 at 3:05:07 PM and does not reflect changes or amendments subsequent to this date and time. The NFHIL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: base map image, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRMS effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

SEE THIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

Without Base Flood Elevation (BFE)
Zone A, V, A99
With BFE or Depth Zone AE, AH, VE, AR
Regulatory Floodway

0.2% Annual Chance Flood Hazard, Area of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone ;

Future Conditions 1% Annual Chance Flood Hazard Zone X

Area with Reduced Flood Risk due to Levee, See Notes, Zone X

Area with Flood Risk due to Levee Zone D

OTHER AREAS OF FLOOD HAZARD

NO SCREEN Area of Minimal Flood Hazard Zone X

Effective LOMRs Area of Undetermined Flood Hazard Zone

GENERAL STRUCTURES

CHANNEL, CULVERT, OR STORM SEWER

Levee, Dike, or Floodwall

CROSS SECTIONS WITH 1% ANNUAL CHANCE

WATER SURFACE ELEVATION

COASTAL TRANSECT

LIMIT OF STUDY

JURISDICTION BOUNDARY

BASE FLOOD ELEVATION LINE (BFE)

OTHER FEATURES

COASTAL TRANSECT BASELINE

PROFILE BASELINE

HYDROGRAPHIC FEATURE

DIGITAL DATA AVAILABLE

MAP PANELS

NO DIGITAL DATA AVAILABLE

UNMAPPED

AREA OF MINIMAL FLOOD HAZARD

Zone X

Zone D

06073C1952.G
5/16/2012
Not Printed

06073C1955.G
5/16/2012
Not Printed

T17S R01E S2

116°50'21.80"W

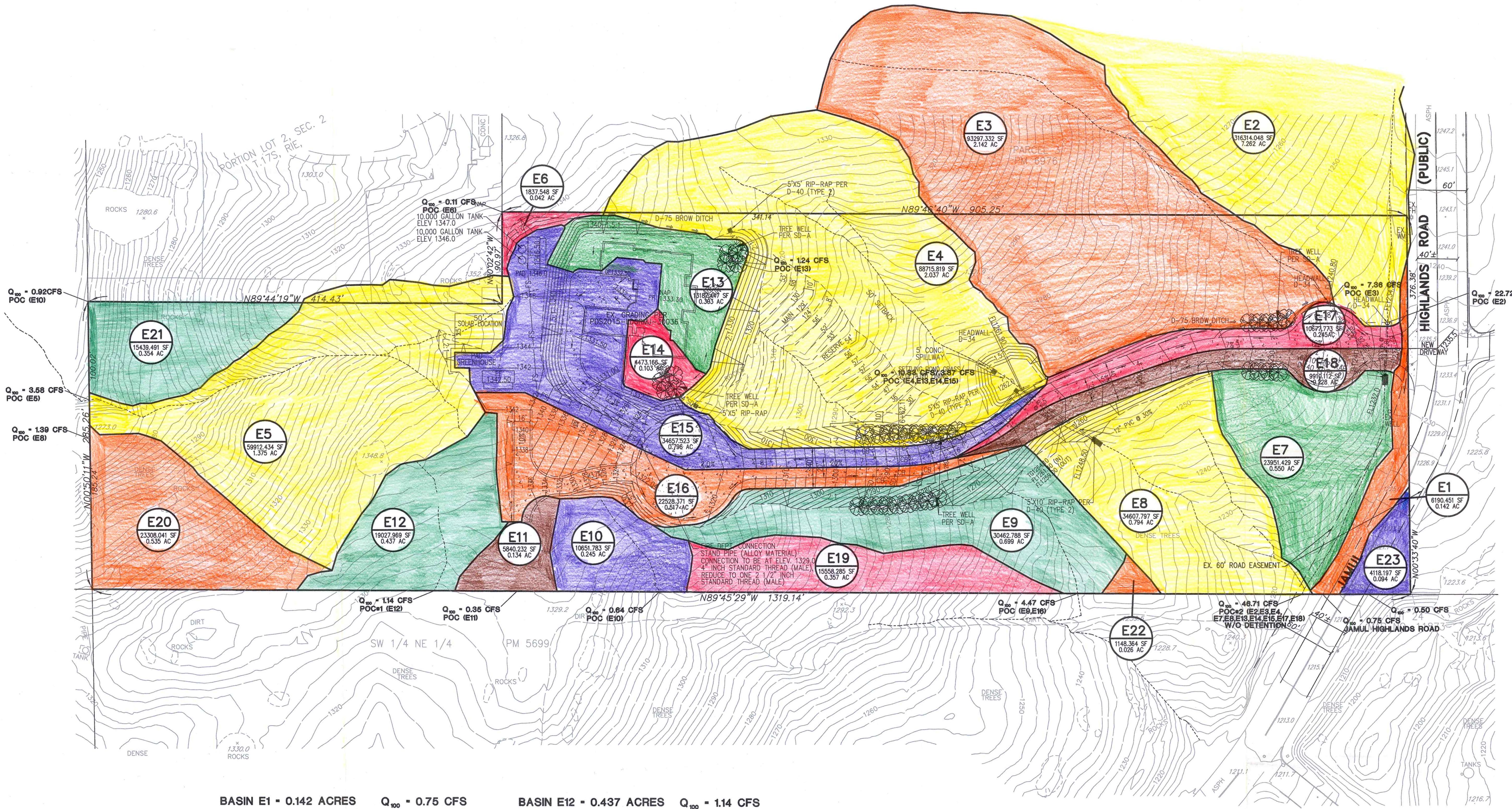
32°43'17.33"N

1:6,000

Feet

250 500 1,000 1,500 2,000

USGS The National Map: Orthoimagery. Date last finished October 2017.



| | |
|-------------------------|-----------------------|
| BASIN E1 - 0.142 ACRES | Q_{100} - 0.75 CFS |
| BASIN E2 - 7.262 ACRES | Q_{100} - 22.72 CFS |
| BASIN E3 - 2.142 ACRES | Q_{100} - 6.70 CFS |
| BASIN E4 - 2.037 ACRES | Q_{100} - 5.31 CFS |
| BASIN E5 - 1.375 ACRES | Q_{100} - 3.58 CFS |
| BASIN E6 - 0.042 ACRES | Q_{100} - 0.11 CFS |
| BASIN E7 - 0.550 ACRES | Q_{100} - 1.72 CFS |
| BASIN E8 - 0.794 ACRES | Q_{100} - 2.07 CFS |
| BASIN E9 - 0.669 ACRES | Q_{100} - 1.82 CFS |
| BASIN E10 - 0.245 ACRES | Q_{100} - 0.64 CFS |
| BASIN E11 - 0.134 ACRES | Q_{100} - 0.35 CFS |
| BASIN E12 - 0.437 ACRES | Q_{100} - 1.14 CFS |
| BASIN E13 - 0.303 ACRES | Q_{100} - 1.24 CFS |
| BASIN E14 - 0.103 ACRES | Q_{100} - 0.41 CFS |
| BASIN E15 - 0.796 ACRES | Q_{100} - 3.87 CFS |
| BASIN E16 - 0.517 ACRES | Q_{100} - 2.65 CFS |
| BASIN E17 - 0.245 ACRES | Q_{100} - 1.32 CFS |
| BASIN E18 - 0.228 ACRES | Q_{100} - 1.41 CFS |
| BASIN E19 - 0.357 ACRES | Q_{100} - 0.93 CFS |
| BASIN E20 - 0.535 ACRES | Q_{100} - 1.39 CFS |
| BASIN E21 - 0.354 ACRES | Q_{100} - 0.92 CFS |
| BASIN E22 - 0.026 ACRES | Q_{100} - 0.07 CFS |
| BASIN E23 - 0.094 ACRES | Q_{100} - 0.50 CFS |

ASSESSOR'S PARCEL NUMBER:
596-152-04

DRAINAGE MAP (EXISTING) FOR:

ROETZHEIM PARCEL MAP

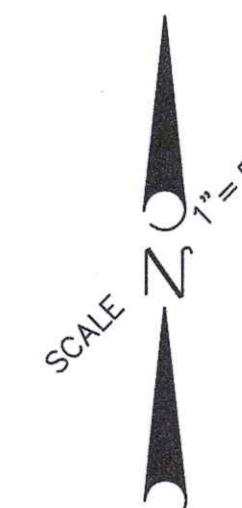


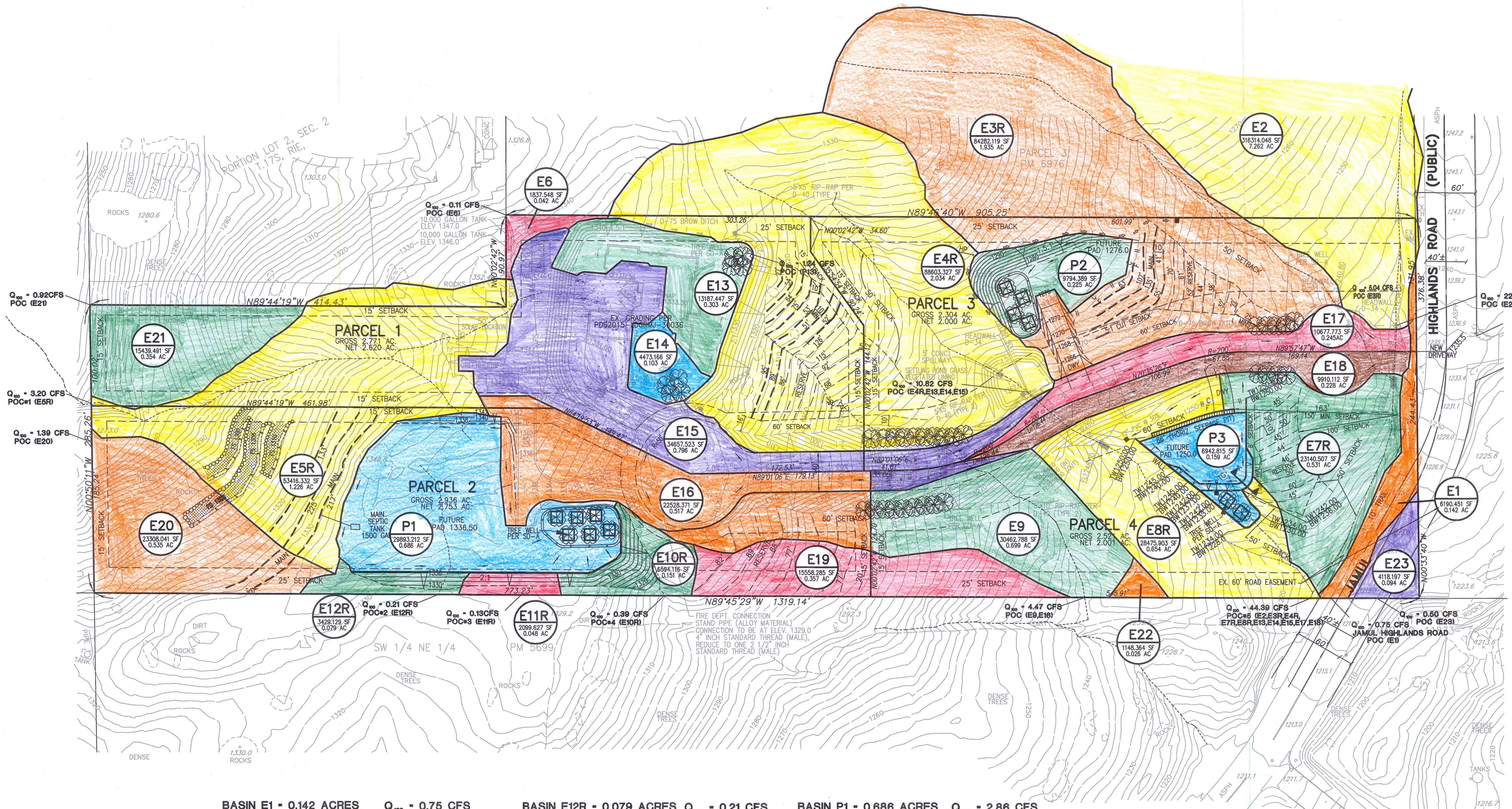
PREPARED FOR:

WILLIAM ROETZHEIM
13518 JAMUL DRIVE
JAMUL, CALIFORNIA 91935
PHONE: (619) 917-4917

LANDMARK ENGINEERING
CORPORATION
3443 Camino Del Rio South
Suite 204
San Diego, CA 92108
(619) 260-0420

| | |
|---|---------------|
| BENCH MARK | |
| DESCRIPTION: 172ECCS3 PER COUNTY CONTROL DATA SHEET | |
| 2" BRASS DISC MARKED 172ECCs3 | |
| LOCATION: IN THE CUL-DE-SAC AT THE OF OLE BURN WAY | |
| RECORD FROM: COUNTY CONTROL DATA SHEET | |
| ELEVATION: 1655.69 | DATUM: NAVD88 |





ASSESSOR'S PARCEL NUMBER:

596-152-04

DRAINAGE MAP (PROPOSED) FOR:

ROETZHEIM PARCEL MAP

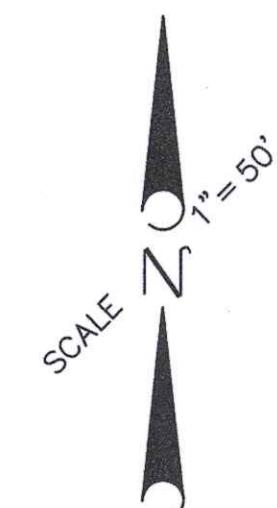


PREPARED FOR:

WILLIAM ROETZHEIM
13518 JAMUL DRIVE
JAMUL, CALIFORNIA 91935
PHONE: (619) 917-4917

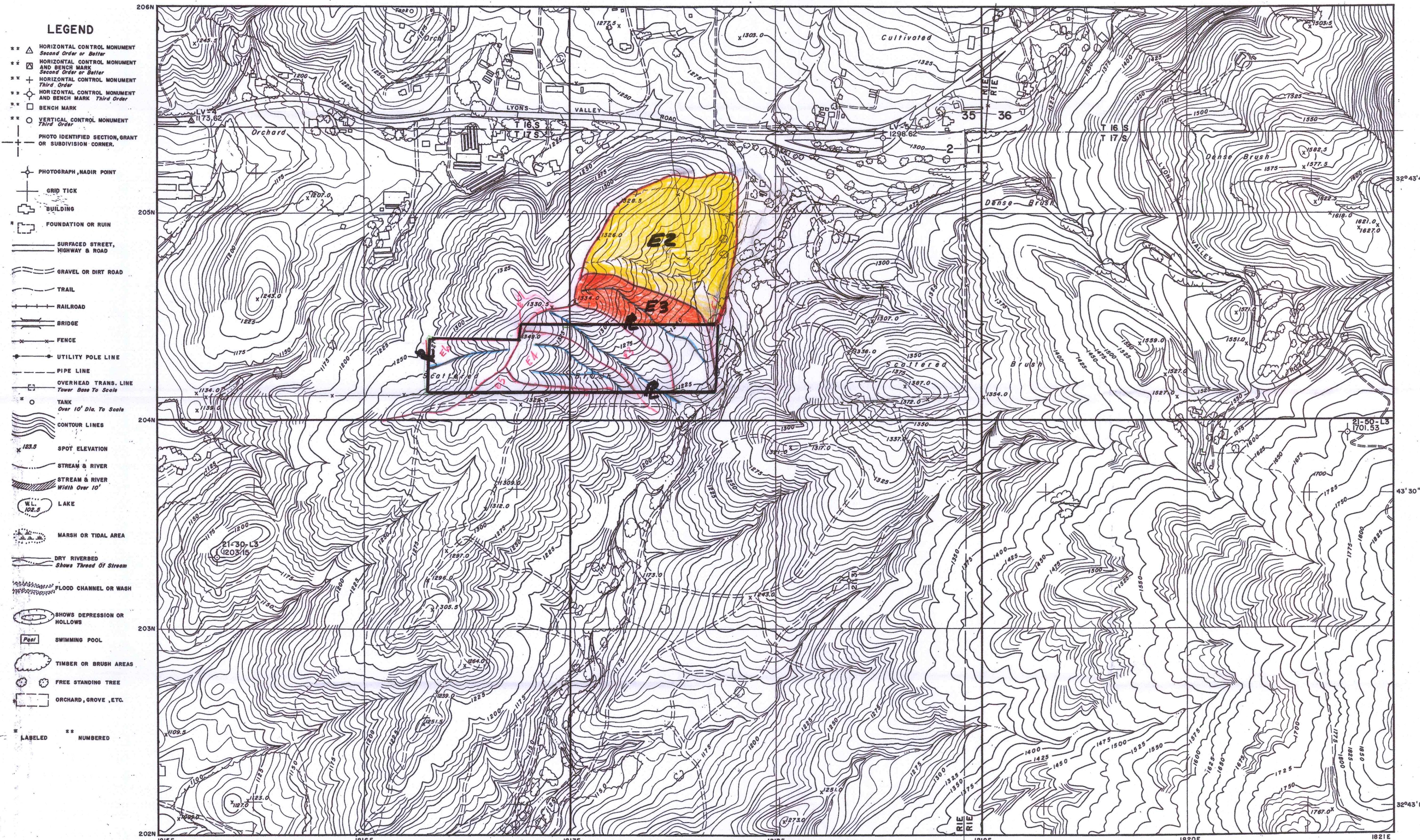
LANDMARK ENGINEERING CORPORATION
3443 Camino Del Rio South
Suite 204
San Diego, CA 92108
(619) 260-0420

| BENCH MARK | |
|--|--|
| DESCRIPTION: 172ECC3 PER COUNTY CONTROL DATA SHEET | |
| 2" BRASS DISC MARKED 172ECC3 | |
| LOCATION: IN THE CUL-DE-SAC AT THE OF OLE BURN WAY | |
| RECORD FROM: COUNTY CONTROL DATA SHEET | |
| ELEVATION: 1655.69 DATUM: NAVD88 | |



COUNTY OF SAN DIEGO

TOPOGRAPHIC SURVEY



PREPARED UNDER THE DIRECTION OF THE COUNTY SURVEYOR
OF THE COUNTY OF SAN DIEGO, CALIFORNIA.
CONTROL BY U.S.C. & G.S., U.S.G.S. AND THE COUNTY OF SAN DIEGO.
NORTH AMERICAN DATUM 1927.

COMPILED BY PHOTOGRAVIMETRIC METHODS
FROM PHOTOGRAPHY DATED AUG. 1964 BY

WESTERN AERIAL SURVEYS
A DIVISION OF H. M. GALLAHER, CIVIL ENGINEER
RIVERSIDE
CALIFORNIA

SCALE 1:2400

200 0 200 400 600 800 1000

CONTOUR INTERVAL 5 FEET

U.S.C. & G.S. DATUM.

ONE THOUSAND FOOT CALIFORNIA RECTANGULAR GRID (ZONE VD)

THE LAST THREE DIGITS OF THE GRID NUMBERS ARE OMITTED

THE RECTANGULAR COORDINATE VALUES ARE SHOWN ON THE SOUTH AND WEST MARGINS

THE GEOGRAPHIC VALUES ARE SHOWN ON THE NORTH AND EAST MARGINS

INDEX TO ADJOINING SHEETS

| 206-1809 | 206-1815 | 206-1821 |
|----------|----------|----------|
| 202-1809 | 202-1815 | 202-1821 |
| 198-1809 | 198-1815 | 198-1821 |

SAN DIEGO COUNTY
CALIFORNIA

EDITION OF 1964

SHEET 202-1815

* OFF SITE EXIST. DRAINAGE MAP